DESIGN SHOWCASE

Programmable Universal Filter Implements C-Message Weighting Function

The C-message filter, which simulates the frequency response of the human ear, is a commonly specified test and measurement filter for voice, audio, and telecommunication applications in the US. In Europe, a close relative is the psophometric noise-weighting filter. You can construct either type by cascading three second-order bandpass sections with a second-order lowpass section. The C-message filter, for example, is shown in Figure 1.

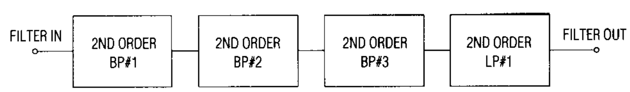


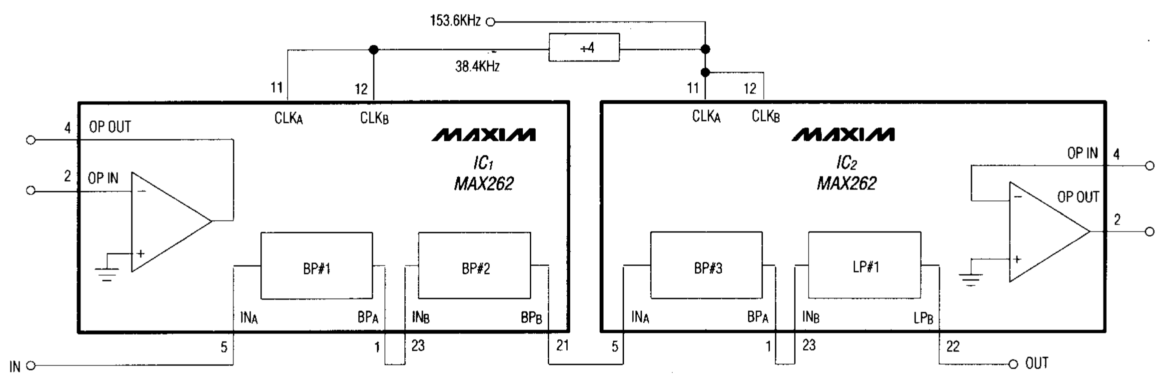
Figure 1. Cascaded, second-order universal filter sections implement a C-message filter.

Dual universal, second-order IC filters provide a compact and efficient means for implementing the circuit of Figure 1. If the IC filters are programmable, switched-capacitor types as shown, you can rapidly implement the C-message, psophometric, or other test filters on demand simply by loading the chips with different sets of coefficients. These coefficients set each 2nd-order section's filter mode, Q, and cutoff or center frequency f_0. The C-message filter has poles only, which are specified by the IEEE Standard 743-1984:

Pole	Value in rad/sec	Value in Hz (f_0)	Q
BP#1	-1502 j1267	312.741	0.6540
BP#2	-2439 j5336	933.761	1.2027
BP#3	-4690 j15267	2541.886	1.7026
LP#1	-4017 j21575	3492.778	2.7316

Figure 2 shows the external connections that configure two filter ICs in the architecture of Figure 1, along with a table of decimal equivalents for the digital coefficients associated with each filter section. These 2nd-order sections establish pole locations in accordance with the f_0 values listed. Each section contains two continuous-time Chebysheff filters whose center frequency can be digitally programmed in 128 steps over the range 1 to 25kHz. Passband ripple is 0.1dB. For maximum signal-to-noise ratio, the signal amplitude at each section output should be as high as possible.

Signal swings are as follows: If you apply 4V to input IN_A on IC_1, output BP_A swings 2.7V, output BP_B swings 1.85V, output BP_A of IC_2 swings 1.6V, and the lowpass output (LP_A of IC_2) swings 3.2V. IC_2 operates in mode 4 instead of mode 1, which provides a gain of 2 instead of 1 for the LP and BP outputs (see data sheet).



MODEA	MODEB	fOA	fOB	QA	QB
1	1	55	2	31	76

MODEA	MODEB	fOA	fOB	QA	QB
4	4	13	3	91	105

Figure 2. The circuit connections and coefficient sets shown enable two programmable, switched-capacitor filter ICs to realize the C-message filter of Figure 1. By loading the ICs with different coefficient sets, you can obtain the European psophometric noise-weighting filter and other test/measurement filters.

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You must bandlimit the filter's input signal to $f_{CLK}/4$ or less, where (in this case) f_{CLK} = 38.4kHz. The uncommitted op amp in IC_1 can provide a 2nd- or 3rd-order lowpass filter for this purpose. The uncommitted op amp in IC_2 can provide a similar lowpass filter for smoothing the output signal.

As an alternative, you can realize the C-message function using one filter IC and an external op amp (Figure 3). This approach lacks flexibility, however. You can no longer switch to other filter functions by electrically reprogramming the circuit.

This circuit realizes the first bandpass (BP#1) in terms of external resistors and capacitors around the uncommitted op amp of IC_1. BP#1, which also serves as an antialiasing filter for the sampling action of IC_1, is an infinite-gain, multiple-feedback bandpass filter with f_0 = 312.74Hz, Q = 0.654, and gain = 0.654. Design procedures for this configuration are available in the literature.

IC_2 implements BP#2 and BP#3 with the same gain and signal levels as in Figure 1. The external op amp with resistors and capacitors implements LP#1, which also serves as the output smoothing filter. Like BP#1, you can design LP#1 as an infinite-gain, multiple-feedback circuit with f_0 = 3492.778Hz, Q = 2.7316, and gain = 2.

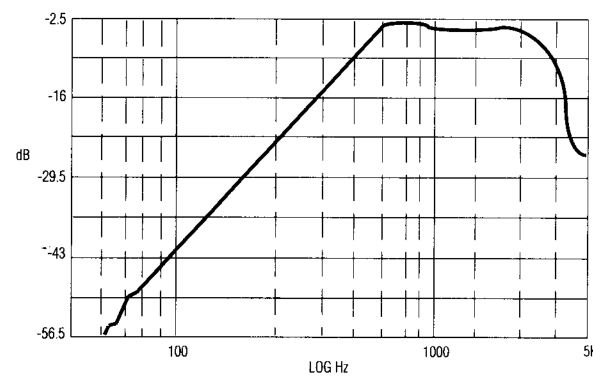
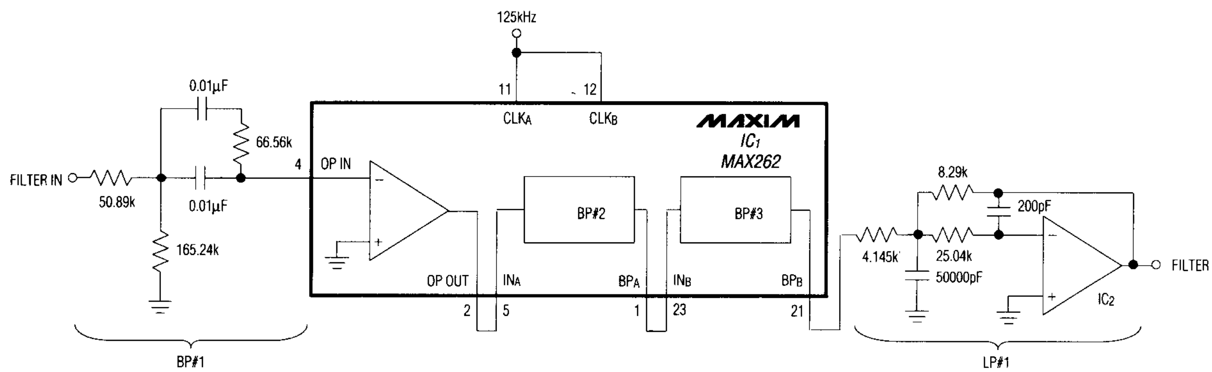


Figure 4. Circuits of Figure 1 and Figure 2 produce the same frequency response.

The 125kHz clock frequency is arbitrary; other values require that you program IC_1 for a different f_{CLK}/f_0 ratio.

In both filter circuits (Figure 1 and Figure 2) the coefficients for f_{0A}, f_{0B}, Q_A, and Q_B were calculated by software available from Maxim (see data sheet). Figure 4 shows the filter transfer function for either realization.

(Circle 6)



CLK_A	CLK_B	$MODE_A$	$MODE_B$	f_{0A}	f_{0B}	Q_A	Q_B
125kHz	125kHz	1	4	N = 61	N = 6	N = 75	N = 91

Figure 3. This circuit, based on one filter IC and an external op amp, produces the same C-message response of Figure 1 but lacks programming flexibility.